

A symbolic-numeric method for the parametric H_∞ loop-shaping design problem

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Abstract—In this paper, we present a symbolic-numeric method for solving the H_∞ loop-shaping design problem for a low order single-input single-output system with parameters. Due to the system parameters, no purely numerical algorithm can indeed solve the problem. Using Gröbner basis techniques and the rational univariate representation of zero-dimensional algebraic varieties, we first give a parametrization of all the solutions of the two algebraic Riccati equations associated with the H_∞ control problem. Then, following the works of [1], [9] on the spectral factorization problem, a certified symbolic-numeric algorithm is obtained for the computations of the positive definite solutions of these two algebraic Riccati equations. Finally, we present a certified symbolic-numeric algorithm which solves the H_∞ loop-shaping design problem for the above class of systems. This algorithm is illustrated with a standard example.

I. INTRODUCTION

Nowadays, automatic control usually consists in the solving of complex problems. As a consequence, this is usually done numerically for a peculiar system and hardware performances are required to handle the underlying numerical computations: the more a system or a problem is refined, i.e., takes into consideration finer dynamics of the physical system or constraints, the more time-computation is required.

An alternative to this approach is to solve these problems symbolically, that is to say to solve the problems corresponding to a certain class of systems. The goal is to have the solution of a control problem for a set of systems depicted by some parameters. Its solution (e.g., the stabilizing corrector) then depends on the system parameters. In what follows, this approach will be called a “*symbolic method*”. One of the greatest benefits of this approach is to simply obtain the solution for a peculiar system belonging to the class of systems by evaluating numerically the system parameters in the closed-form solution. Since only evaluation operations are required, this task can be achieved for a cheap computational cost.

The purpose of this paper is to develop a symbolic method for the H_∞ loop-shaping design problem [8], [15], [17] for linear systems containing parameters. This synthesis problem yields the computation of a stabilizing controller which

takes into account robustness objectives in the frequency domain (e.g., stability margins) and the modeling of different transfer functions via perturbations. Practically, H_∞ control provides a natural *compromise* between the performance and the robustness of a control-loop. The desired performance properties and robustness conditions can be obtained by “*weighting*” the plant transfer function, which results in a “*weighted plant*”. But shaping a high performance closed-loop system will degrade its robustness.

On the practical point of view, such an approach is interesting in the design stage of a project, when a designer needs to know if the global design of its system has a chance to reach the specifications, or if a global rework is needed. As the global design is likely to change at some stage, the engineer has to quickly provide a range of performances and robustness that the closed-loop system could achieve in order to *choose the appropriate global design*. This approach is also interesting in *adaptive control* where the controller depends on the measurement of variables or parameters (e.g., a mechanical mode) and has to be re-computed in real time (i.e., quickly relative to the dynamics of the system). As the technologies of embedded processors are not powerful enough to compute H_∞ optimization problems in real time, the symbolic approach developed in this paper is justified.

Solving the H_∞ control problem for a system with parameters requires solving an Algebraic Riccati Equation (ARE), whose resolution was studied in [7] using *Gröbner basis techniques*. A method to solve an H_∞ control problem was proposed in [9] based on properties of the spectral factorization of the Hamiltonian matrix associated with the ARE [10]. In this article, a different method is proposed by means of the study of the polynomial system defined by an ARE (Section III). A *rational univariate representation* of the solutions of this polynomial system is given (Section IV). In Section V, the equivalence between our method and the one developed in [9] is shown. In Section VI, an algorithm is given to compute the optimal solution to the H_∞ control problem by means of certified root isolation methods. Finally, in Section VII, a standard example illustrates our method.

II. THE STANDARD H_∞ -CONTROL PROBLEM

In this paper, we will consider a single-input single-output (SISO) finite-dimensional linear system (Figure 1) defined by $\hat{y}_1 = G \hat{e}_1$, where the transfer function G is given by

$$G := \frac{c_n s^n + c_{n-1} s^{n-1} + \dots + c_1 s + c_0}{a_n s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0}, \quad (1)$$

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$a_i, c_i \in \mathbb{R}$ for $i = 0, \dots, n$ and n is the order of G . In what follows, to get a strictly proper transfer function G , we set:

$$a_n := 1, \quad c_n := 0, \quad c_{n-1} \neq 0. \quad (2)$$

Let us consider its controller canonical form defined by the following state-space representation

$$\begin{aligned} \dot{x} &= A x + B e_1, \quad y_1 = C x, \\ A &:= \begin{pmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \ddots & \vdots \\ \vdots & \vdots & \ddots & \ddots & 0 \\ 0 & 0 & \dots & 0 & 1 \\ -a_0 & -a_1 & \dots & -a_{n-2} & -a_{n-1} \end{pmatrix} \in \mathbb{R}^{n \times n}, \\ B &:= (0 \dots 0 \ 1)^T \in \mathbb{R}^{n \times 1}, \\ C &:= (c_0 \dots c_{n-1}) \in \mathbb{R}^{1 \times n}. \end{aligned} \quad (4)$$

Let $K \in \mathbb{R}(s)$ be a rational controller and let us consider the closed-loop system defined in Figure 1. If we denote the sensitivity transfer function by $S := (1 + G K)^{-1}$, then:

$$\begin{pmatrix} e_1 \\ y_1 \end{pmatrix} = \begin{pmatrix} S & K S \\ S G & K S G \end{pmatrix} \begin{pmatrix} u_1 \\ u_2 \end{pmatrix}.$$

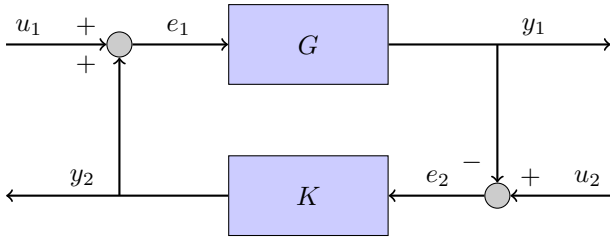


Fig. 1. Control scheme

Let us consider the following standard problem.

Robust Control Problem (RCP): Given $\gamma > 0$, find a controller K which stabilizes G (i.e., such that the rational transfer functions S , $K S$ and $S G$ are proper and stable) and is such that:

$$\left\| \begin{pmatrix} S & K S \\ S G & K S G \end{pmatrix} \right\|_{\infty} < \gamma. \quad (5)$$

For more details, see [8], [17], [6], [15] and the references therein. The RCP yields a compromise between the performance of the closed-loop system and the robustness with respect to the perturbations u_1 and u_2 .

We briefly state a standard result of H_{∞} -control theory.

Theorem 1: [8, Cor. 5.1], [17, Ch. 18], [6, Th. 3.2] Let (A, B, C) be a controllable and observable state-space representation (3) of the transfer function G defined by (1). Then, the minimal value of γ for (5) is given by

$$\gamma_{\min} = \sqrt{1 + \lambda_{\max}(\mathcal{Y} \mathcal{X})}, \quad (6)$$

where λ_{\max} is the greatest eigenvalue of $\mathcal{Y} \mathcal{X}$, and \mathcal{X} and \mathcal{Y} are respectively the *real positive definite* matrices,

solutions of the following two *Algebraic Riccati Equations* (ARE):

$$\mathcal{R} := X A + A^T X - X B B^T X + C^T C = 0, \quad (7)$$

$$\tilde{\mathcal{R}} := Y A^T + A Y - Y C^T C Y + B B^T = 0. \quad (8)$$

For $\gamma > \gamma_{\min}$, a controller K satisfying RCP is defined by

$$\dot{z} = A_{\gamma} z + B_{\gamma} e_2, \quad y_2 = C_{\gamma} z,$$

with the following notations:

$$\begin{cases} Z_{\gamma} := (I_n + \mathcal{Y} \mathcal{X} - \gamma^2 I_n)^{-1}, \\ A_{\gamma} := A - B B^T \mathcal{X} + \gamma^2 Z_{\gamma} \mathcal{Y} C^T C, \\ B_{\gamma} := -\gamma^2 Z_{\gamma} \mathcal{Y} C^T, \\ C_{\gamma} := B^T \mathcal{X}. \end{cases}$$

We note that $\mathcal{R}^T = \mathcal{R}$ and $\tilde{\mathcal{R}}^T = \tilde{\mathcal{R}}$. In this article, we denote by \mathcal{X} (resp. \mathcal{Y}) the positive definite solution of \mathcal{R} (resp. $\tilde{\mathcal{R}}$). The next lemma shows that (8) is a consequence of (7) for SISO systems.

Lemma 1: We have $\mathcal{Y} := \mathcal{Q} \mathcal{X} \mathcal{Q}$ where $\mathcal{Q} = \mathcal{Q}^T$ is defined by:

$$\mathcal{Q}^{-1} := \mathcal{P} = (\mathcal{P}_1 \dots \mathcal{P}_n), \quad (9)$$

$$\begin{cases} \mathcal{P}_n^T := C, \\ \mathcal{P}_{n-1}^T := C (A + a_{n-1} I_n), \\ \dots \\ \mathcal{P}_2^T := C (A^{n-2} + a_{n-1} A^{n-3} + \dots + a_2 I_n), \\ \mathcal{P}_1^T := C (A^{n-1} + a_{n-1} A^{n-2} + \dots + a_1 I_n). \end{cases}$$

Corollary 1: Denoting by $\lambda_{\star}(M) := \max_i |\lambda_i(M)|$ the greatest absolute value of the real eigenvalues λ_i 's of a matrix M , we have

$$\gamma_{\min} = \sqrt{1 + \lambda_{\max}(\mathcal{Y} \mathcal{X})} = \sqrt{1 + \lambda_{\star}^2(\mathcal{Q} \mathcal{X})}. \quad (10)$$

In this paper, we focus on the computation of \mathcal{X} in the case where the a_i 's and c_j 's are unknown parameters and not fixed numerical values. In particular, numerical algorithms for the computation of the positive definite solutions of ARE cannot be used. We have to consider symbolic methods to take into account the parameters a_i 's and c_j 's.

III. POLYNOMIAL SYSTEM DESCRIPTION OF AN ARE

Firstly, we study the equation $\mathcal{R} = 0$. For $1 \leq i \leq j \leq n$, we denote by $x_{i,j}$ the entries of X and we set $x_{i,0} = 0$.

Proposition 1: The equation $\mathcal{R} = 0$, defined by (7), is equivalent to the following system of $\frac{n(n+1)}{2}$ polynomial equations in the $\frac{n(n+1)}{2}$ unknowns $\{x_{i,j}\}_{1 \leq i \leq j \leq n}$:

$$\begin{aligned} &-(x_{i,n} + a_{i-1})(x_{j,n} + a_{j-1}) \\ &+ x_{i,j-1} + x_{i-1,j} + a_{i-1} a_{j-1} + c_{i-1} c_{j-1} = 0, \end{aligned} \quad (11)$$

$$1 \leq i \leq j \leq n.$$

If we introduce the following notations

$$\begin{cases} k < 0, & b_k := 0, \\ 0 \leq k \leq n-1, & b_k := x_{k+1,n} + a_k, \\ k = n, & b_k := 1, \\ k > n, & b_k := 0, \end{cases} \quad (12)$$

then the diagonal elements of the matrix \mathcal{R} yield:

$$1 \leq i \leq n, \quad 2x_{i-1,i} = 2x_{i,i-1} = b_{i-1}^2 - (a_{i-1}^2 + c_{i-1}^2). \quad (13)$$

Furthermore, using (11) and (12), the i^{th} row of X can be deduced from the $(i-1)^{\text{th}}$ row, which allows us to write $x_{i,j-1}$ in terms of $x_{i-1,j}$ which itself can be expressed in terms of $x_{i-2,j+1}, \dots$. If we note

$$\theta_m := \sum_{k=0}^m (-1)^k (a_{i-1-k} a_{j-1+k} + c_{i-1-k} c_{j-1+k}), \quad (14)$$

then after m substitutions, we obtain for $1 \leq i < j \leq n-m$:

$$\begin{aligned} x_{i,j-1} &= (-1)^{m+1} x_{i-1-m,j+m} \\ &+ \sum_{k=0}^m (-1)^k b_{i-1-k} b_{j-1+k} - \theta_m. \end{aligned} \quad (15)$$

We distinguish two halting conditions in the induction:

- 1) We reach an element of the form $x_{i-1-m,j+m} = x_{0,j+m} = 0$ for $m = i-1$. In this case, note that we have $1 \leq j+m \leq n$.
- 2) We reach an element of the form $x_{i-1-m,j+m} = x_{i-1-m,n}$ for $m = n-j$. In this case, note that we have $1 \leq i-1-m \leq n$.

The first condition is equivalent to:

$$2 \leq i+j \leq n+1.$$

By reaching this limit, one obtains the following expression:

$$\begin{aligned} \forall (i,j) \in \mathbb{N}^2, \quad i < j, \quad 2 \leq i+j \leq n+1, \\ x_{i,j-1} &= \sum_{k=0}^{i-1} (-1)^k b_{i-1-k} b_{j-1+k} - \theta_{i-1}. \end{aligned} \quad (16)$$

The second condition is equivalent to:

$$n+1 < i+j \leq 2n+1.$$

By reaching this limit, using $x_{i+j-n-1,n} = b_{i+j-n-2} - a_{i+j-n-2} = b_{i+j-n-2} b_n - a_{i+j-n-2} a_n$ (see (2) and (12)), we obtain the following expression:

$$\begin{aligned} \forall (i,j) \in \mathbb{N}^2, \quad i < j, \quad n+1 < i+j \leq 2n+1, \\ x_{i,j-1} &= \sum_{k=0}^{n-j+1} (-1)^k b_{i-1-k} b_{j-1+k} - \theta_{n-j+1}. \end{aligned} \quad (17)$$

Hence, the entries $x_{i,j}$ of X can be explicitly expressed in terms of the b_k 's defined in (12), i.e., up to constant, in terms of the elements of the last column $x_{k,n}$ of X . The results can be summarized in the following proposition.

Proposition 2: For $k = 1 \dots n$, we set $x_{k,0} = x_{0,k} := 0$, and for $(i,j) \in \mathbb{N}^2$, we define:

$$\begin{cases} N := i-1, & 2 \leq i+j \leq n+1, \\ N := n-j+1, & n+1 < i+j \leq 2n+1. \end{cases}$$

The elements of X solution of (7) are determined only by the b_k 's as follows

$$\begin{cases} 1 \leq k \leq n, & x_{k,n} = b_{k-1} - a_{k-1}, \\ 1 \leq i < j \leq n, & x_{i,j-1} = \sum_{k=0}^N (-1)^k b_{i-1-k} b_{j-1+k} - \theta_N, \end{cases} \quad (18)$$

where θ_N is defined by (14).

We note that for $i = 1$, using $x_{1,0} = 0$, (13) then yields:

$$\mathcal{B}_0 := b_0^2 - (a_0^2 + c_0^2) = 0. \quad (19)$$

For $i \neq 1$, $x_{i-1,i}$ appears twice in (13) and (16) or (17). Thus, combining (13) and (18) for $i = j = k+1$, we obtain a polynomial system of $n-1$ equations in $n-1$ unknowns $\{b_i\}_{1 \leq i \leq n-1}$. This system, denoted by \mathcal{B} , is defined by

$$\mathcal{B} := \{\mathcal{B}_k = 0\}_{0 \leq k \leq n-1}, \quad (20)$$

where the polynomials \mathcal{B}_k are defined by

$$\begin{cases} \mathcal{B}_0 := b_0^2 - d_0, \\ \mathcal{B}_k := b_k^2 + 2 \sum_{m=1}^N (-1)^m b_{k-m} b_{k+m} - d_{2k}, \\ 1 \leq k \leq n-1, \end{cases} \quad (21)$$

and the constants d_{2k} are defined by

$$\begin{cases} d_0 := a_0^2 + c_0^2, \\ d_{2k} := 2 \sum_{m=1}^N (-1)^m (a_{k-m} a_{k+m} + c_{k-m} c_{k+m}) \\ \quad + a_k^2 + c_k^2, \\ d_{2n} := 1, \\ 1 \leq k \leq n-1, \end{cases} \quad (22)$$

where:

$$\begin{cases} N := k, & 1 \leq k \leq \frac{n-1}{2}, \\ N := n-k, & \frac{n-1}{2} < k \leq n-1. \end{cases}$$

Remark 1: We point out that the parameters a_i 's and c_j 's appear only in the constant terms of the \mathcal{B}_k 's (compare with (11)), which highly simplifies the study of (20).

If the d_{2k} 's are fixed, then the polynomial system (22) defines all the transfer functions G (see (1)) which give the same ARE. The study of this algebraic variety will be studied in details in a future publication.

Let $\mathbb{K} := \mathbb{Q}(d_0, \dots, d_{2n})$, $\overline{\mathbb{K}}$ its algebraic closure and $\mathbb{K}' := \mathbb{Q}(a_0, \dots, a_{n-1}, c_0, \dots, c_{n-1})$. Using *Gröbner basis techniques* (see, e.g., [4] and the references therein), we can now state results on (20).

Proposition 3: The polynomial system \mathcal{B} given by (20) and defined over $R := \mathbb{K}[b_0, \dots, b_{n-1}]$ is zero-dimensional (i.e., $\mathcal{A} := R/\langle \mathcal{B} \rangle$, where $\langle \mathcal{B} \rangle := \{\sum_{i=1}^n r_i \mathcal{B}_i \mid r_i \in R\}$ is the ideal of R generated by \mathcal{B} , is a finite-dimensional \mathbb{K} -vector space¹). The dimension of the \mathbb{K} -vector space \mathcal{A} is 2^n .

¹For any rational (complex) values of the parameters d_i 's, the system (21) has a finite number of complex solutions.

Moreover, \mathcal{B} is a *reduced Gröbner basis* of $\langle \mathcal{B} \rangle$ with respect to the *degree reverse lexicographic (DRL) order* $b_{n-1} \succ \dots \succ b_0$.

Proof: According to the *Buchberger criterion* (see, e.g., [4] and the references therein), \mathcal{B} is a *Gröbner basis* with respect to the DRL order $b_{n-1} \succ \dots \succ b_0$. Moreover, this Gröbner basis is reduced according to [4, ch. 2, §7, Definition 4]. Since the *leading monomial* of each polynomial in the Gröbner basis \mathcal{B} is of the form b_k^2 , by [4, ch. 5, §6, Theorem 4], \mathcal{A} is a finite-dimensional \mathbb{K} -vector space. Using the notation $b^\alpha := \prod_{i=0}^{n-1} b_i^{\alpha_i}$ where $\alpha := (\alpha_0, \dots, \alpha_{n-1}) \in \mathbb{N}^n$, a basis of \mathcal{A} is defined by $\{b^\alpha\}_{\alpha \in \llbracket 0,1 \rrbracket^n}$. Finally, the dimension of \mathcal{A} is equal to 2^n . ■

Remark 2: Combining Propositions 3 and 2, we get that the polynomial system $\mathcal{R} = 0$ associated with an ARE of a SISO system (1) is a finite-dimensional \mathbb{K} -vector space of dimension 2^n with basis $\{b^\alpha\}_{\alpha \in \llbracket 0,1 \rrbracket^n}$ (see (12)).

IV. PARAMETRIZATION OF THE SOLUTIONS

In Section III, we show that we can reduce the problem of computing the solutions of the ARE equation $\mathcal{R} = 0$ to those of a zero-dimensional system \mathcal{B} . This system is given by its Gröbner basis \mathcal{B} with respect to the DRL order. From the end-user point of view, a convenient way to express the solutions of such a system is to use a *Rational Univariate Representation (RUR)* [12], [13], i.e., a one-to-one mapping

$$\begin{aligned} V(\langle \mathcal{B} \rangle) &\longrightarrow V(\langle p \rangle) \\ b = (b_0, \dots, b_{n-1}) &\longmapsto \xi \\ \left(\frac{p_0(\xi)}{q(\xi)}, \dots, \frac{p_{n-1}(\xi)}{q(\xi)} \right) &\longleftarrow \xi, \end{aligned} \quad (23)$$

between the solutions of the system \mathcal{B} defined by

$$V(\langle \mathcal{B} \rangle) := \left\{ b \in \overline{\mathbb{K}}^n \mid r(b) = 0, \forall r \in \langle \mathcal{B} \rangle \right\},$$

and the roots of a univariate polynomial p . The explicit formulas for $p, p_0, \dots, p_{n-1}, q \in \mathbb{K}[t]$ is given thereafter. In order to achieve the one-to-one condition, the above representation is computed with respect to a *separating element* t , that is a linear combination $t := \sum_{i=0}^{n-1} u_i b_i$ of the b_i 's, that takes different values when evaluated at different points of $V(\langle \mathcal{B} \rangle)$.

Generically, i.e. for almost any value of the parameters, the system \mathcal{B} admits $t := b_{n-1}$ as a separating element. In that case, the above representation has the following form

$$\begin{cases} p(b_{n-1}) = 0, \\ b_{n-1} = b_{n-1}, \\ b_{n-2} = \frac{p_{n-2}(b_{n-1})}{q(b_{n-1})}, \\ \dots \\ b_0 = \frac{p_0(b_{n-1})}{q(b_{n-1})}, \end{cases} \quad (24)$$

where $p, p_0, \dots, p_{n-1}, q$ are in $\mathbb{K}[b_{n-1}]$ and p and q are coprime polynomials, i.e., $\gcd(p, q) = 1$.

For instance, given a generic value of the parameters, using (24), we can compute certified numerical approximations of

the real solutions by first isolating the real roots of p by means of intervals [14], and then substituting these intervals into the expressions $\frac{p_i(b_{n-1})}{q(b_{n-1})}$ for $i = 0 \dots n-2$ to get the corresponding isolating intervals for the b_i 's.

From the computation point of view, a RUR of \mathcal{B} can be obtained using the algorithm given in [13]. This algorithm requires the knowledge of a basis of $\mathcal{A} := R/\langle \mathcal{B} \rangle$ (e.g., $\{b^\alpha\}_{\alpha \in \llbracket 0,1 \rrbracket^n}$; see the proof of Proposition 3) and a reduction algorithm which computes normal forms modulo the ideal $\langle \mathcal{B} \rangle$. In order to explicitly characterize the polynomials appearing in the RUR, we first have to define the multiplication \mathbb{K} -endomorphism of \mathcal{A} defined by $r \in R$ by

$$\begin{aligned} m_r : \mathcal{A} &\longrightarrow \mathcal{A} \\ \bar{a} &\longmapsto \overline{ra}, \end{aligned}$$

where \bar{a} denotes the residue class of $a \in R$ in \mathcal{A} (i.e., modulo $\langle \mathcal{B} \rangle$). A representative of \bar{a} is the normal form of a with respect to the Gröbner basis \mathcal{B} . Using the basis $\{b^\alpha\}_{\alpha \in \llbracket 0,1 \rrbracket^n}$, the \mathbb{K} -endomorphism m_r can be defined by means of a matrix $M_r \in \mathbb{K}^{2^n \times 2^n}$. Then, p is the characteristic polynomial of $M_{b_{n-1}}$. Moreover, if

$$\bar{p}(b_{n-1}) := \frac{p}{\gcd\left(p, \frac{dp}{db_{n-1}}\right)} = \sum_{i=0}^d v_i b_{n-1}^{d-i} \in \mathbb{K}[b_{n-1}]$$

denotes the *square-free part* of p and if we note

$$H_j(b_{n-1}) := \sum_{i=0}^j v_i b_{n-1}^{j-i} \in \mathbb{K}[b_{n-1}], \quad j = 0, \dots, d-1,$$

then, for $k = 0, \dots, n-2$, we can define:

$$\begin{cases} q(b_{n-1}) := \sum_{i=0}^{d-1} \text{Trace}(M_{b_{n-1}}^i) H_{d-i-1}(b_{n-1}), \\ p_k(b_{n-1}) := \sum_{i=0}^{d-1} \text{Trace}(M_{b_k} M_{b_{n-1}}^i) H_{d-i-1}(b_{n-1}). \end{cases}$$

For more details, see [12], [13]. Note that the polynomials $p, p_0, \dots, p_{n-1}, q$ defining a RUR (23) are not unique. The above formulas give us a way to compute the RUR. But the polynomials appearing are usually not the shortest ones. For instance, for small orders (i.e., $n < 5$), a RUR can easily be obtained by direct computations yielding simple expressions.

Finally, if b_{n-1} is a separating element and the ideal $\langle \mathcal{B} \rangle$ is *radical* (i.e., $\sqrt{\langle \mathcal{B} \rangle} := \{r \in R \mid \exists l \in \mathbb{N} : r^l \in \langle \mathcal{B} \rangle\} = \langle \mathcal{B} \rangle$), a similar representation can be computed by performing a change of order for the Gröbner basis (passing from the DRL order to the *lexicographic order* $b_0 \succ \dots \succ b_{n-1}$) [13]. However, the size of the outputs is then much more larger than the one given by a RUR [13], a fact increasing the computational cost.

For instance, on our regular machine (Intel Core i7 2.60 GHz processor and 16 Go of RAM), we can compute the RUR of \mathcal{B} for $n = 6$ with all the parameters a_i 's and c_j 's in 20 minutes Maple 18 CPU time. By comparison, a similar computation based on a change of order for the Gröbner basis \mathcal{B} did not finish after 3 days (due to a lack of memory).

Remark 3: If q is square-free (i.e., the discriminant $\text{Disc}(q) \in \mathbb{K}$ of q is not zero), then the ideal $\langle \mathcal{B} \rangle$ is radical and b_{n-1} is a separating element. In a future work, the conditions of non degeneracy will be further studied.

Finally, combining (24) and (18), all the entries $x_{i,j}$ of X can be expressed in terms of $b_{n-1} = x_{n,n} - a_{n-1}$ (see (12)).

Remark 4: Note that the above effective method yields the explicit resolution of an ARE for a general SISO system with parameters. It can be used to study many standard problems (optimal control and estimation problems such as H_∞ or H_2 optimal control, LQ control, model order reduction, Kalman filtering, ...) for SISO system with parameters.

Once an explicit expression of the solutions of $\mathcal{R} = 0$ is known (see (24)), the objective is then to characterize the positive definite one, i.e. \mathcal{X} , among the 2^n solutions.

Proposition 4: [8] Let (A, B) be a controllable pair and (C, A) an observable pair. Then, there exists a unique real positive definite solution \mathcal{X} of (7).

According to Proposition 4, if numerical values of the a_i 's and c_j 's are given, then a unique real symmetric definite positive solution \mathcal{X} of (7) exists. Hence, from the 2^n complex solutions of (20), using (18), we have to find the real one which yields the unique real symmetric definite positive solution \mathcal{X} of (7).

V. FROM ARE TO SPECTRAL FACTORIZATION

Another way to obtain a positive definite solution of \mathcal{R} is by using the invariant subspaces of the Hamiltonian matrix \mathcal{H} defined by:

$$\mathcal{H} := \begin{pmatrix} A & -B B^T \\ -C^T C & -A^T \end{pmatrix} \in \mathbb{K}^{2n \times 2n}.$$

Using (4), the computation of the characteristic polynomial of \mathcal{H} , denoted by $f(\lambda) := \det(\mathcal{H} - \lambda I_n)$, gives:

$$f(\lambda) = (-1)^n \sum_{i=0}^n \sum_{j=0}^n \delta_{i,j} \lambda^{i+j}, \quad \delta_{i,j} := (-1)^i (a_i a_j + c_i c_j).$$

We have:

$$f(\lambda) := \lambda^{2n} + (-1)^n \sum_{k=0}^{n-1} \left(\sum_{\substack{0 \leq i,j \leq n \\ i+j=2k}} \delta_{i,j} \lambda^{2k} + \sum_{\substack{0 \leq i,j \leq n \\ i+j=2k+1}} \delta_{i,j} \lambda^{2k+1} \right). \quad (25)$$

Note that the coefficient of f of degree $2k+1$ in λ vanishes for $k=0, \dots, n-1$. Moreover, some coefficients of λ^{2k} appear twice and after tedious computation, we obtain

$$f(\lambda) := \sum_{k=0}^n (-1)^{n+k} d_{2k} \lambda^{2k}, \quad (26)$$

where d_{2k} is defined in (22). As a consequence, f is an even polynomial, i.e. $f(-\lambda) = f(\lambda)$.

The even property of f leads to the *spectral factorization problem* which consists in finding a polynomial

$$g(\lambda) := \sum_{k=0}^n \beta_k \lambda^k \quad (27)$$

such that:

$$f(\lambda) = (-1)^n g(\lambda) g(-\lambda). \quad (28)$$

Hence, we have:

$$f(\lambda) = (-1)^n \sum_{i=0}^n \sum_{j=0}^i (-1)^i \beta_i \beta_j \lambda^{i+j}. \quad (29)$$

Replacing $\delta_{i,j}$ by $(-1)^i \beta_i \beta_j$ in (25), we obtain (29). After similar tedious computation as the ones done to get (26), using the change of variable $i := k - m$ and $j := k + m$, we obtain

$$f(\lambda) = \sum_{k=0}^n (-1)^{n+k} \left(\beta_k^2 + 2 \sum_{m=1}^N (-1)^m \beta_{k-m} \beta_{k+m} \right) \lambda^{2k}, \quad (30)$$

$$\begin{cases} N := k, & 1 \leq k \leq \frac{n-1}{2}, \\ N := n-k, & \frac{n-1}{2} < k \leq n-1. \end{cases}$$

Combining (26) and (30), we finally obtain

$$1 \leq k \leq n, \quad d_{2k} = \beta_k^2 + 2 \sum_{m=1}^N (-1)^m \beta_{k-m} \beta_{k+m},$$

which coincides with (21) with $\beta_k = b_k$ for $k=1, \dots, n$. We find again that the problem of the spectral factorization of the characteristic polynomial of the Hamiltonian matrix is equivalent to searching for solutions of an ARE. We now study a way to choose $b_{n-1} = \beta_{n-1}$ to get the unique positive definite solution \mathcal{X} of (7).

In the sequel, *the parameters are fixed to generic values*. Since f is even, if λ is a solution of f , then so is $-\lambda$. Let $\{\alpha_i\}_{i=1, \dots, n}$ be the roots of f with positive real parts (see (26)). Given g satisfying (28), then α_i is a solution of $g(\lambda) = 0$ or $g(-\lambda) = 0$, i.e., $\pm \alpha_i$ is a root of g . Since β_{n-1} is a sum of the roots of g , we get $\beta_{n-1} = \sum_{i=1}^n \epsilon_i \alpha_i$ where $\epsilon_i \in \{-1, 1\}$. Now, if $\{\nu_k\}_{k=1, \dots, 2^n}$ is the set of complex solutions of \mathcal{B} , where $\nu_k := (\nu_{k,0}, \dots, \nu_{k,n-1})$, $\epsilon_{k,i} \in \{-1, 1\}$, and $\nu_{k,n-1}$ is the n^{th} coordinate of ν_k , using $\beta_{n-1} = b_{n-1}$ (see above), then we get: $\nu_{k,n-1} = \sum_{i=1}^n \epsilon_{k,i} \alpha_i$, $1 \leq k \leq 2^n$. Moreover, we have

$$\sigma := \sum_{i=1}^n \alpha_i = \max_{k \in \{1, \dots, 2^n\}} \nu_{k,n-1}, \quad (31)$$

For more details, see [10]. We obtain the following theorem.

Theorem 2 ([10]): The positive definite solution \mathcal{X} of $\mathcal{R} = 0$ corresponds to the real solution ν_k of \mathcal{B} such that $b_{n-1}(\nu_k)$ is maximal.

VI. CERTIFIED COMPUTATION OF γ_{\min}

As stated in Theorem 1, an optimal solution of the RCP is given by (10). Using the RUR (24) of \mathcal{B} and (18), we can express the entries $x_{i,j}$ (resp., $y_{i,j}$) of X (resp., Y) in terms of $b_{n-1} = x_{n,n} - a_{n-1}$, and then we compute the characteristic polynomial of $\mathcal{Q}X$:

$$h(\lambda, b_{n-1}) := \det(\mathcal{Q}X - \lambda I_n).$$

The numerator of h , denoted by h_* , belongs to $\mathbb{K}'[\lambda, b_{n-1}]$. Hence, the problem of computing γ_{\min} is equivalent to that of the maximal real solution of $h_*(\lambda, \sigma) = 0$, where σ is defined by (31) (i.e., the maximal real root of p). We note again that σ defines the solutions \mathcal{X} and \mathcal{Y} .

This problem can be tackled using purely numerical methods. For instance, one approach consists in first isolating the root σ of p by means of an interval and then substituting this interval into $h_*(\lambda, b_{n-1})$ and isolate again in order to find λ_* . However, such numerical methods fail to provide a *certified output* (see [5], [14]), especially when $h_*(\lambda, \sigma)$ is not square-free in λ . In order to achieve a certification, we can instead consider the following *triangular system*

$$\begin{cases} p(b_{n-1}) = 0, \\ h_*(\lambda, b_{n-1}) = 0, \end{cases} \quad (32)$$

and compute a certified numerical approximation of the solution (σ, λ_*) [5], [14].

There exist several exact methods for solving (32) and thus for deducing the desired solution (σ, λ_*) . We can mention the algorithm of [3] which uses some *separation bounds* in order to isolate the roots of the polynomial $h_*(\lambda, b_{n-1})$ over a root of p , or the algorithm given in [2] which requires the computation of a decomposition of (32) into a set of square-free triangular systems so that for any root α of p the polynomial $h_*(\lambda, \alpha)$ is square-free.

We now use again the idea developed in Section IV and compute a RUR of the solutions of (32). For a well chosen separating element $\tau := u_1 b_{n-1} + u_2 \lambda$, these solutions can be expressed by:

$$\begin{cases} v(\tau) = 0, \\ b_{n-1} = \frac{v_1(\tau)}{w(\tau)}, \\ \lambda = \frac{v_2(\tau)}{w(\tau)}. \end{cases} \quad (33)$$

Finally, in order to obtain the solution (σ, λ_*) , it is sufficient to isolate the real roots of v , evaluate the resulting intervals in the expressions $\frac{v_1(\tau)}{w(\tau)}$ and $\frac{v_2(\tau)}{w(\tau)}$, which yields boxes isolating the solutions, and finally choose the one that satisfies the requirement (i.e., the maximal λ obtained from the maximal b_{n-1}).

Getting λ_* , we deduce $\gamma_{\min} := \sqrt{1 + \lambda_*^2}$, which allows us to compute an optimal H_∞ controller by Theorem 1.

Finally, we recapitulate the above approach for solving the RCP by outlining an algorithm.

Algorithm 1:

- 1) Using Proposition 3, compute \mathcal{B} .
- 2) Compute a RUR (24) of the ideal $\langle \mathcal{B} \rangle$.
- 3) Using Proposition 2, compute X in terms of b_{n-1} .
- 4) Compute \mathcal{Q} defined by (9).
- 5) Compute $\mathcal{Q}X$ and the numerator of its characteristic polynomial h_* .
- 6) Compute a RUR of (32) to get (33).
- 7) Isolate the solutions of (33) by means of 2D-boxes and select the desired box corresponding to (σ, λ_{\max}) .

- 8) Compute $\gamma_{\min} := \sqrt{1 + \lambda_*^2}$.
- 9) Compute $\mathcal{Y} := \mathcal{Q} \mathcal{X} \mathcal{Q}$.
- 10) Compute a controller satisfying the RCP using Theorem 1.

VII. EXAMPLE: A TWO-MASS-SPRING SYSTEM

We illustrate the above approach on the two-mass-spring problem (Figure 2) considered in [16], [15], which mathematical model is similar to the one of a 2-dimensional gyrostabilized sight².

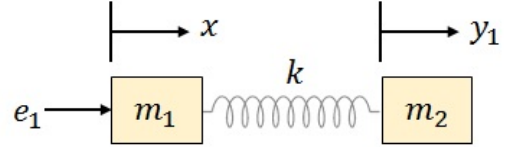


Fig. 2. Two-mass-spring system

Two masses m_1 and m_2 are linked by a spring of stiffness k . With the notations of Figure 1, we study the displacement of m_2 , denoted by y_1 , while m_1 is excited by a force e_1 . We consider the transfer function of the *physical plant*

$$P := \frac{c}{s^2(s^2 + a_2)}, \quad c := \frac{k}{m_1 m_2}, \quad a_2 := \frac{m_1 + m_2}{m_1 m_2} k,$$

between the input e_1 and the output y_1 . As in [15, §2.6, §4], we consider a weight $w > 0$ and define the *fictive plant* by

$$G := wP = \frac{c_0}{s^2(s^2 + a_2)}, \quad c_0 := w c > 0, \quad a_2 > 0,$$

which will be used in Algorithm 1. As seen above, we can design the loop-shaping controller K stabilizing G . From this controller K , we finally get a controller $C := wK$ robustly stabilizing the physical plant P .

For the system G , the polynomials \mathcal{B}_k 's defined in Proposition 3, are given by

$$\begin{cases} \mathcal{B}_0 := b_0^2 - d_0 = 0, \\ \mathcal{B}_1 := b_1^2 - 2b_0 b_2 - d_2 = 0, \\ \mathcal{B}_2 := b_2^2 - 2b_1 b_3 + 2b_0 - d_4 = 0, \\ \mathcal{B}_3 := b_3^2 - 2b_2 - d_6 = 0, \end{cases} \quad (34)$$

where the constants d_{2k} 's are defined by:

$$d_0 := c_0^2, \quad d_2 := 0, \quad d_4 := a_2^2, \quad d_6 := -2a_2. \quad (35)$$

Using $\mathcal{B}_0 = 0$, we notice that b_0 is completely determined by d_0 . We then assume that its value is known. If $b_3 = 0$, then the last equation of (34) yields $b_2 = a_2$, and thus the last but one gives $b_0 = 0$, i.e., $c_0 = 0$ by means of the first one, which shows that $G = 0$. Since in the sequel we suppose that $G \neq 0$, and thus, $b_3 \neq 0$, using (24), a RUR of the system $\{\mathcal{B}_1 = 0, \mathcal{B}_2 = 0, \mathcal{B}_3 = 0\}$ for the separating element b_3 can easily be obtained by direct computations

$$\begin{cases} b_1 = \frac{b_3^4 + 4a_2 b_3^2 + 8b_0}{8b_3}, \\ b_2 = \frac{1}{2} b_3^2 + a_2, \\ b_3 = b_3, \end{cases} \quad (36)$$

²A gyrostabilized sight is a system of cameras controlled in rotation by motors and gyroscopes.

where b_3 satisfies the following polynomial equation:

$$p(b_3) := b_3^8 + 8a_2 b_3^6 + 16(a_2^2 - 3b_0) b_3^4 - 64a_2 b_0 b_3^2 + 64b_0^2 = 0. \quad (37)$$

Note that $b_0 = \pm c_0$ (recall that $c_0 > 0$). Applying the change of variable $\tau = (8c_0)^{-1/2} b_3^2$, we have:

$$c_0 \tau^4 + \sqrt{8c_0} a_2 \tau^3 + 2(a_2^2 \mp 3c_0) \tau^2 \mp \sqrt{8c_0} a_2 \tau + c_0 = 0. \quad (38)$$

The latter polynomial is (anti-)palindromic, so we can apply the change of variable $\varsigma := \tau \mp \tau^{-1}$ in order to get:

$$p_s(\varsigma) := c_0 \varsigma^2 + 2\sqrt{2c_0} a_2 \varsigma + 2a_2^2 \mp 4c_0 = 0. \quad (39)$$

The discriminant of (39) is $\pm 16c_0^2$. When $b_0 = -c_0$, the discriminant is negative, and the solutions of (39) are not real. Therefore, we consider the case $b_0 = c_0$. Then, p_s has two distinct real roots, which are:

$$\begin{cases} \varsigma_+ := -\sqrt{\frac{2a_2^2}{c_0}} + 2, \\ \varsigma_- := -\sqrt{\frac{2a_2^2}{c_0}} - 2, \end{cases} \quad \varsigma_- < 0, \quad \varsigma_+ > \varsigma_-, \quad |\varsigma_-| > |\varsigma_+|.$$

Then, τ verifies $\tau^2 - \tau\varsigma - 1 = 0$ which discriminant is $\varsigma^2 + 4 > 0$. Its solutions are given by:

$$\begin{cases} \tau_+ := \frac{1}{2} \left(\varsigma_{\pm} + \sqrt{\varsigma_{\pm}^2 + 4} \right), \\ \tau_- := \frac{1}{2} \left(\varsigma_{\pm} - \sqrt{\varsigma_{\pm}^2 + 4} \right), \end{cases} \quad \varsigma_{\pm} \in \{\varsigma_+, \varsigma_-\}.$$

Then all the roots of (38) are real. It is clear that τ_+ is the maximal real root of (38), which leads to the following expression of σ , maximal real root of p :

$$\sigma := \sqrt{2} \sqrt{(\sqrt{2c_0} - a_2) + \sqrt{(\sqrt{2c_0} - a_2)^2 + 2c_0}}. \quad (40)$$

Using Proposition 2 (see (18)), the matrix X is defined by

$$X := \begin{pmatrix} c_0 b_1 & c_0 b_2 & c_0 b_3 & c_0 \\ c_0 b_2 & -c_0 b_3 + b_1 b_2 & b_1 b_3 - c_0 & b_1 \\ c_0 b_3 & b_1 b_3 - c_0 & b_2 b_3 - b_1 & b_2 - a_2 \\ c_0 & b_1 & b_2 - a_2 & b_3 \end{pmatrix},$$

where b_1 and b_2 are defined by (36). By (9), we have:

$$\mathcal{Q} := \begin{pmatrix} 0 & 0 & 0 & c_0^{-1} \\ 0 & 0 & c_0^{-1} & 0 \\ 0 & c_0^{-1} & 0 & -a_2 c_0^{-1} \\ c_0^{-1} & 0 & -a_2 c_0^{-1} & 0 \end{pmatrix}.$$

The numerator h_* of the characteristic polynomial of $\mathcal{Q}\mathcal{X}$ divided by c_0^2 , i.e., $h_s := h_* c_0^{-2}$, is defined by:

$$h_s(\lambda, b_3) = 4c_0 \lambda^4 - \alpha(b_3) \lambda^3 + \beta(b_3) \lambda^2 + \alpha(b_3) \lambda + 4c_0, \quad (41)$$

$$\alpha := b_3^4 + 8c_0, \quad \beta := -2(b_3^4 + 4c_0). \quad (42)$$

Noticing that h_s is *anti-palindromic* and considering the change of variable $t := \lambda - \lambda^{-1}$ ($\lambda = 0$ is not a root of h_s since its constant term $4c_0$ is non-zero), h_s can then be rewritten as:

$$h_s(t, b_3) = 4c_0 t^2 - \alpha(b_3) t - 2b_3^4. \quad (43)$$

The roots of the latter polynomial are then given by:

$$\begin{cases} t_+(b_3) := \frac{1}{8c_0} \left(\alpha(b_3) + \sqrt{\alpha(b_3)^2 + 32c_0 b_3^4} \right), \\ t_-(b_3) := \frac{1}{8c_0} \left(\alpha(b_3) - \sqrt{\alpha(b_3)^2 + 32c_0 b_3^4} \right). \end{cases}$$

The roots of h_* are then of the form:

$$\begin{cases} \lambda_+ := \frac{1}{2} \left(t_{\pm} + \sqrt{t_{\pm}^2 + 4} \right), \\ \lambda_- := \frac{1}{2} \left(t_{\pm} - \sqrt{t_{\pm}^2 + 4} \right), \end{cases} \quad t_{\pm} \in \{t_+, t_-\}.$$

Let us now determine the root of h_* of greatest absolute value. Since we have $t_+ t_- = -\frac{2b_3^4}{4c_0} < 0$ and $t_+ > t_-$, t_- is necessarily negative while t_+ is positive. Furthermore, since $t_+ + t_- = \frac{\alpha(b_3)}{4c_0} > 0$, then we have $t_+ = |t_+| > -t_-$, i.e., $|t_+| > |t_-|$. The root of h_* of greatest absolute value is then defined by:

$$\lambda_* := \frac{1}{2} \left(t_+ + \sqrt{t_+^2 + 4} \right). \quad (44)$$

Hence, the minimal γ is obtained using (40):

$$\gamma_{\min}(\sigma) := \sqrt{1 + \left(\frac{1}{2} \left(t_+(\sigma) + \sqrt{t_+(\sigma)^2 + 4} \right) \right)^2}.$$

Using the explicit formula given in Theorem 1, we can explicitly compute a robust stabilizing controller C of P .

Figure 3 shows the plot of the function γ_{\min} in terms of the values of the parameters a_2 and c_0 .

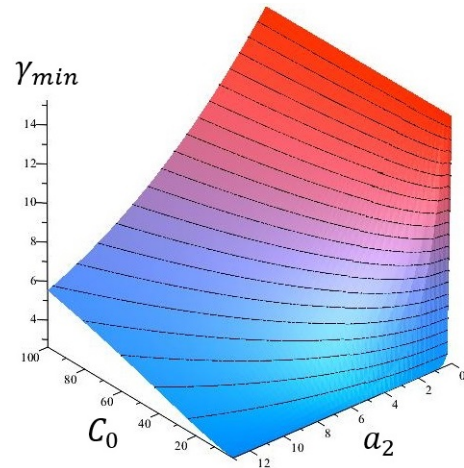


Fig. 3. $\gamma_{\min} = \Gamma(a_2, c_0)$

The weight w can be seen as a scalar tuning parameter. In particular, it can be chosen so that $\gamma_{\min} = 3$, which ensures

a good gain margin Δ_G and a good phase margin Δ_Φ :

$$\begin{cases} \Delta_G(P, C) = \Delta_G(G, K) \geq \frac{1 + \gamma_{\min}^{-1}}{1 - \gamma_{\min}^{-1}} = 6 \text{ dB}, \\ \Delta_\Phi(P, C) = \Delta_\Phi(G, K) \geq 2 \arcsin(\gamma_{\min}^{-1}) = 39^\circ. \end{cases}$$

For more details, see, e.g., [15, Th.2.10].

For instance, for $\gamma_{\min} = 3$, w_{opt} is obtained by choosing:

$$w_{\text{opt}} = \frac{4a_2^2}{197261828370049c} \left(6246072 + 3625216\sqrt{2} - \sqrt{90755864194240 + 67218229682478\sqrt{2}} \right)^2.$$

As a consequence, we obtain the optimal H_∞ auto-tuned controller $C_{\text{opt}}(\gamma_{\min}, c, a_2)$. By on-line identification of the modal frequency a_2 , the optimal controller $C_{\text{opt}}(\gamma_{\min}, c, a_2)$ can be computed in real-time by a simple embedded calculator (which does not have to contain optimization routines).

Remark 5: Since we usually cannot solve by radicals univariate polynomials of degree larger than or equal to 4, we have to use the symbolic-numeric method described in Algorithm 1. Let us show how to compute the second RUR at Step 6 of Algorithm 1 for the above example. We can first compute a RUR of the polynomial system defined by p and h_s given by (37) and (43) with $T = b_3^2$, i.e.:

$$\begin{cases} T^4 + 8a_2T^3 + 16(a_2^2 - 3c_0)T^2 - 64a_2c_0T + 64c_0^2 = 0, \\ 4c_0t^2 - (T^2 + 8c_0)t - 2T^2 = 0. \end{cases} \quad (45)$$

After some eliminations, we obtain $T = \delta(t)\theta^{-1}(t)$, where

$$\begin{cases} \delta(t) = -c_0t^4 + (-4a_2^2 + 16c_0)t^3 - 8c_0t^2 \\ \quad + 16(a_2^2 - 4c_0)t - 16c_0, \\ \theta(t) = 2a_2(t^3 - 2t^2 - 12t - 8), \end{cases} \quad (46)$$

and t satisfies the following polynomial equation:

$$\begin{aligned} c_0^2t^8 - 8c_0(a_2^2 + 4c_0)t^7 + 16(a_2^4 + 17c_0^2)t^6 \\ - 32c_0(a_2^2 + 4c_0)t^5 - 32(4a_2^4 + 61c_0^2)t^4 \\ + 128c_0(a_2^2 + 4c_0)t^3 + 256(a_2^4 + 17c_0^2)t^2 \\ + 512c_0(a_2^2 + 4c_0)t + 256c_0^2 = 0. \end{aligned} \quad (47)$$

Substituting $t = \lambda - \lambda^{-1}$ into (46) and (47), we obtain a RUR for the polynomial system defined by (37) and (41). For explicit values of a_2 and c_0 , root isolation techniques can then be used to compute the H_∞ controller. For instance, for $a_2 = 10$ and $c_0 = 1$, solving (47) by means of isolation techniques yields 16 intervals for the λ 's (use, e.g., the Maple command `RootFinding[Isolate]`). Using interval arithmetic (see, e.g., the `IntpakX` Maple Package) and (46), these intervals leads to 16 intervals for the T 's. We then have to choose the one with the greatest absolute value as stated in Section VI and we get:

$$\lambda_* \in [2.4369432563, 2.4369442170].$$

This interval yields the interval for $\sigma := \max(b_3) = \sqrt{T_{\text{max}}}$:

$$\sigma \in [0.4810240843, 0.4810241306].$$

For $a_2 = 10$ and $c_0 = 1$, using (40) and (44), we obtain $\sigma \approx 0.481024117$ and $\lambda_* \approx 2.4369437154$.

VIII. CONCLUSION

In this paper, we have initiated a new symbolic-numeric method for solving the H_∞ loop-shaping design problem for low order SISO systems with parameters. To do that, we first showed that solving an ARE of size $n \times n$ is equivalent to solving a certain zero-dimensional polynomial system of n equations in n unknowns, and that a RUR can be used to parametrize all its real solutions. Then, using a result of spectral factorization [10], we showed how to solve an H_2 control problem. The computation of the controller satisfying the robust 4-block problem requires a second RUR computation and symbolic/numeric root isolation techniques.

When the univariate polynomials of the two RUR can be reduced to polynomials of degrees less than or equal to 4, then an explicit formula of the H_∞ controller can be obtained. The dependence of this controller to the system parameters can then be analytically studied, which is useful, e.g., in the applications to gyro-stabilized sights. For higher order systems, a certified numerical root isolation technique has to be used to compute the H_∞ controller.

Further works include the search for tractable RURs in order to deal with highest order systems. Furthermore, our approach will be applied to small order models of gyro-stabilized sights to develop an adaptive control scheme.

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